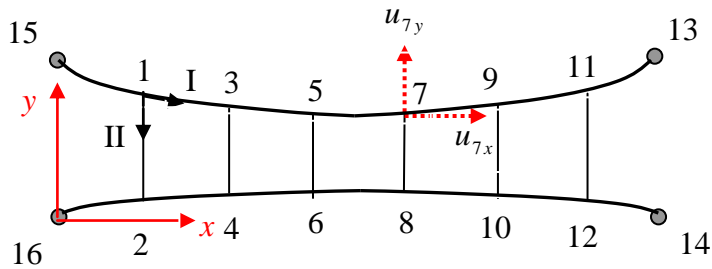


STRUCTURA MATRICII DE RIGIDITATE – Exemplu

Considerăm o fermă-cablu , cu numerotarea din figură a nodurilor.



Vectorul deplasărilor de nod va fi:

$$\mathbf{U} = \begin{bmatrix} \mathbf{U}_1 \\ \vdots \\ \mathbf{U}_2 \\ \vdots \\ \mathbf{U}_{12} \end{bmatrix} = \begin{bmatrix} u_{1x} \\ u_{1y} \\ \vdots \\ u_{2x} \\ u_{2y} \\ \vdots \\ u_{12x} \\ u_{12y} \end{bmatrix} = \begin{bmatrix} u_1 \\ u_2 \\ u_3 \\ u_4 \\ \vdots \\ u_{23} \\ u_{24} \end{bmatrix}$$

Drumurile orientate, incidente într-un nod, se definesc astfel:

I – În lungul cablului, sensul spre dreapta;

II – Vertical descendent.

Tabelul elementelor incidente în nod, pe drumurile I, II, este:

Nod	Drum incident în nod	
	I	II
1	15-1 1-3	0 1-2
2	16-2 2-4	1-2 0
3	1-3 3-5	0 3-4
Etc.

Notă

Elementele de cablu sunt notate acum, pentru o identificare mai simplă, prin $NI-NF$ (nod_inițial - nod_final); în practică, elementele se numerotează cu indici consecutivi
 1 – Numărul_elementelor.

■

Ecuțiile de echilibru de nod sunt (6-2, §6.2, Teoria de calcul):

$$\left[\begin{array}{cccc} -\mathbf{A}_{K-1}^I & \vdots & -\mathbf{A}_{K-1}^{II} & \vdots & \mathbf{A}_{K-1}^I + \mathbf{A}_{K-1}^{II} + \mathbf{A}_K^I + \mathbf{A}_K^{II} & \vdots & -\mathbf{A}_K^I & \vdots & -\mathbf{A}_K^{II} \end{array} \right] \begin{bmatrix} \Delta \mathbf{U}_{K-1,I} \\ \Delta \mathbf{U}_{K-1,II} \\ \Delta \mathbf{U}_K \\ \Delta \mathbf{U}_{K+1,I} \\ \Delta \mathbf{U}_{K+1,II} \end{bmatrix} = \mathbf{P}_K - \mathbf{f}_K$$

Reamintim că, în aceste ecuații, indicele K notează:

- În \mathbf{A}_K^J : *elementul orientat* $K \rightarrow K + 1$, pe drumul J .
- În $\Delta \mathbf{U}_K$: *nodul* K .

În $\Delta \mathbf{U}_{K\pm 1,J}$: indicii $K - 1, J$ și $K + 1, J$ notează (relativ la nodul K): nodul “în urmă”, și respectiv nodul ”înainte”, pe drumul J .

Ecuția anterioară se scrie, explicit:

$$\left[\begin{array}{cccc} -\mathbf{A}_{K-1,K}^I & \vdots & -\mathbf{A}_{K-1,K}^{II} & \vdots & \mathbf{A}_{K-1,K}^I + \mathbf{A}_{K-1,K}^{II} + \mathbf{A}_{K,K+1}^I + \mathbf{A}_{K,K+1}^{II} & \vdots & -\mathbf{A}_{K,K+1}^I & \vdots & -\mathbf{A}_{K,K+1}^{II} \end{array} \right] \begin{bmatrix} \Delta \mathbf{U}_{K-1,I} \\ \Delta \mathbf{U}_{K-1,II} \\ \Delta \mathbf{U}_K \\ \Delta \mathbf{U}_{K+1,I} \\ \Delta \mathbf{U}_{K+1,II} \end{bmatrix} = \mathbf{P}_K - \mathbf{f}_K$$

Astfel, avem:

- Nodul 1:

$$\left[-\mathbf{A}_{15-1} \quad \mathbf{0} \quad \mathbf{A}_{15-1} + \mathbf{0} + \mathbf{A}_{1-3} + \mathbf{A}_{1-2} \quad -\mathbf{A}_{1-3} \quad -\mathbf{A}_{1-2} \right] \begin{bmatrix} \Delta \mathbf{U}_{15} \\ \mathbf{0} \\ \Delta \mathbf{U}_1 \\ \Delta \mathbf{U}_3 \\ \Delta \mathbf{U}_2 \end{bmatrix} = \mathbf{P}_1 - \mathbf{f}_1$$

Țineți cont că $\mathbf{U}_{15} = \mathbf{0}$ (nodul 15 este fix), și deci, $\Delta \mathbf{U}_{15} = \mathbf{0}$.

Ecuția efectivă, cu deplasările ordonate în ordinea 1–n, va fi:

$$\left[-\mathbf{A}_{15-1} \quad \mathbf{0} \quad \mathbf{A}_{15-1} + \mathbf{0} + \mathbf{A}_{1-3} + \mathbf{A}_{1-2} \quad -\mathbf{A}_{1-2} \quad -\mathbf{A}_{1-3} \right] \begin{bmatrix} \mathbf{0} \\ \mathbf{0} \\ \Delta \mathbf{U}_1 \\ \Delta \mathbf{U}_2 \\ \Delta \mathbf{U}_3 \end{bmatrix} = \mathbf{P}_1 - \mathbf{f}_1$$

- Nodul 2:

$$\left[-\mathbf{A}_{16-2} \quad -\mathbf{A}_{1-2} \quad \mathbf{A}_{16-2} + \mathbf{0} + \mathbf{A}_{2-4} + \mathbf{A}_{1-2} \quad -\mathbf{A}_{2-4} \quad \mathbf{0} \right] \begin{bmatrix} \Delta \mathbf{U}_{16} \\ \Delta \mathbf{U}_1 \\ \Delta \mathbf{U}_2 \\ \Delta \mathbf{U}_4 \\ \mathbf{0} \end{bmatrix} = \mathbf{P}_2 - \mathbf{f}_2$$

- Nodul 3:

$$\left[-\mathbf{A}_{1-3} \quad \mathbf{0} \quad \mathbf{A}_{1-3} + \mathbf{0} + \mathbf{A}_{3-5} + \mathbf{A}_{3-4} \quad -\mathbf{A}_{3-5} \quad -\mathbf{A}_{3-4} \right] \begin{bmatrix} \Delta \mathbf{U}_1 \\ \mathbf{0} \\ \Delta \mathbf{U}_3 \\ \Delta \mathbf{U}_5 \\ \Delta \mathbf{U}_4 \end{bmatrix} = \mathbf{P}_3 - \mathbf{f}_3$$

- Etc.

Ecuția matriceală de echilibru (ecuația 6-3 din § 6.2 – Teoria de calcul) este

$$\mathbf{A} \cdot \Delta \mathbf{U} = \mathbf{P} - \mathbf{f}$$

În care:

$$\Delta \mathbf{U} = \begin{bmatrix} \Delta \mathbf{U}_1 \\ \Delta \mathbf{U}_2 \\ \vdots \\ \Delta \mathbf{U}_{12} \end{bmatrix} = \begin{bmatrix} \Delta u_{1x} \\ \Delta u_{1y} \\ \Delta u_{2x} \\ \Delta u_{2y} \\ \vdots \\ \Delta u_{12x} \\ \Delta u_{12y} \end{bmatrix} = \begin{bmatrix} \Delta u_1 \\ \Delta u_2 \\ \Delta u_3 \\ \Delta u_4 \\ \vdots \\ \Delta u_{23} \\ \Delta u_{24} \end{bmatrix}; \quad \mathbf{P} - \mathbf{f} = \begin{bmatrix} \mathbf{P}_1 - \mathbf{f}_1 \\ \mathbf{P}_2 - \mathbf{f}_2 \\ \vdots \\ \mathbf{P}_{12} - \mathbf{f}_{12} \end{bmatrix}.$$

Structura matricii de rigiditate tangente \mathbf{A} , este:

$$\mathbf{A} = \begin{bmatrix} \mathbf{A}_{11} & -\mathbf{A}_{12} & -\mathbf{A}_{13} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ -\mathbf{A}_{21} & \mathbf{A}_{22} & -\mathbf{A}_{23} & -\mathbf{A}_{24} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ -\mathbf{A}_{31} & -\mathbf{A}_{32} & \mathbf{A}_{33} & -\mathbf{A}_{34} & -\mathbf{A}_{35} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & -\mathbf{A}_{42} & -\mathbf{A}_{43} & \mathbf{A}_{44} & -\mathbf{A}_{45} & -\mathbf{A}_{46} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ & & & & \ddots & & & & & & & & \\ & & & & & & & & & & & & \\ & & & & & & & & & & & & \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & -\mathbf{A}_{11,9} & -\mathbf{A}_{11,10} & \mathbf{A}_{11,11} & -\mathbf{A}_{11,12} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & -\mathbf{A}_{12,10} & -\mathbf{A}_{12,11} & \mathbf{A}_{12,12} \end{bmatrix}$$

În care:

$$\mathbf{A}_{11} = \mathbf{A}_{15-1} + \mathbf{A}_{1-3} + \mathbf{A}_{1-2};$$

$$\mathbf{A}_{12} = \mathbf{A}_{1-2}; \quad \mathbf{A}_{13} = \mathbf{A}_{1-3}$$

$$\mathbf{A}_{22} = \mathbf{A}_{16-2} + \mathbf{A}_{2-4} + \mathbf{A}_{1-2}$$

$$\mathbf{A}_{21} = \mathbf{A}_{12}; \quad \mathbf{A}_{23} = \mathbf{0}; \quad \mathbf{A}_{24} = \mathbf{A}_{2-4}$$

$$\mathbf{A}_{33} = \mathbf{A}_{1-3} + \mathbf{A}_{3-5} + \mathbf{A}_{3-4}$$

$$\mathbf{A}_{31} = \mathbf{A}_{1-3}; \quad \mathbf{A}_{32} = \mathbf{A}_{23} = \mathbf{0}; \quad \mathbf{A}_{34} = \mathbf{A}_{3-4}; \quad \mathbf{A}_{35} = \mathbf{A}_{3-5}$$

Etc.

De exemplu, explicit:

$$\mathbf{A}_{1-3} = \begin{bmatrix} A_{1-3}^{11} & A_{1-3}^{21} \\ A_{1-3}^{12} & A_{1-3}^{22} \end{bmatrix},$$

în care:

$$A_{1-3}^{LM} = \frac{1}{\Delta s_{1-3}^0} [\delta_{LM} T_{1-3}^0 + (\lambda_{1-3}^0 A_{1-3}^0 Y_{1-3}^0 - T_{1-3}^0) \frac{V_{1-3}^L V_{1-3}^M}{|\mathbf{V}_{1-3}|^3}]; \quad L, M = 1, 2 \quad (L, M = x, y)$$

■

Exemplu numeric

Ferma-cablu, cu:

- Deschidere: $2l = 42m$ (7 panouri \times 6m)
- Săgeți: $f_s = 3.5m$ (superior); $f_i = 2.1m$ (inferior)
- Înălțime: $h = 7.6m$
- Modul de elasticitate: $Y = 16500kN/cm^2$
- Arii: $A_s = 20cm^2$; $A_i = 12cm^2$; $A_m = 0.6cm^2$
- Pretensionare – cablu inferior: $H_i^0 = 318kN$
- Încărcare: $P = 10kN$, vertical în jos, în nodurile superioare.

Matricea de rigiditate – în configurația de echilibru (rezultat NELSAS)

Este listat numai triunghiul superior al matricii (matrice simetrică).

Matricea de rigiditate (Triunghiul superior) (kN/m); Semi-latime de banda: 6

101011.7	-24055.02	-3.328782	1.270904
-52142.03	9995.621		
0.000000	0.000000	0.000000	0.000000
0.000000	0.000000		
0.000000	0.000000	0.000000	0.000000
0.000000	0.000000		
0.000000	0.000000	0.000000	0.000000
0.000000	0.000000		
8098.644	1.270904	-2041.976	9995.621
-1963.201	0.000000		
0.000000	0.000000	0.000000	0.000000
0.000000	0.000000		

0.000000	0.000000	0.000000	0.000000
0.000000	0.000000		
0.000000	0.000000	0.000000	0.000000
0.000000			
64100.52	9009.456	0.000000	0.000000
-32427.00	-3653.484		
0.000000	0.000000	0.000000	0.000000
0.000000	0.000000		
0.000000	0.000000	0.000000	0.000000
0.000000	0.000000		
0.000000	0.000000	0.000000	0.000000
0.000000			
3457.006	0.000000	0.000000	-3653.484
-459.8479	0.000000		
0.000000	0.000000	0.000000	0.000000
0.000000	0.000000		
0.000000	0.000000	0.000000	0.000000
0.000000	0.000000		
0.000000	0.000000	0.000000	0.000000
0.000000			
106432.1	-15202.19	-5.326690	3.293367
-54284.75	5203.277		
0.000000	0.000000	0.000000	0.000000
0.000000	0.000000		
0.000000	0.000000	0.000000	0.000000
0.000000	0.000000		
0.000000	0.000000	0.000000	0.000000
0.000000			
5782.588	3.293367	-3274.865	5203.277
-544.5213	0.000000		
0.000000	0.000000	0.000000	0.000000
0.000000	0.000000		
0.000000	0.000000	0.000000	0.000000
0.000000	0.000000		
0.000000	0.000000	0.000000	0.000000
0.000000			
65326.99	5502.978	0.000000	0.000000
-32894.66	-1852.787		
0.000000	0.000000	0.000000	0.000000
0.000000	0.000000		
0.000000	0.000000	0.000000	0.000000
0.000000	0.000000		
0.000000	0.000000	0.000000	0.000000
0.000000			
3886.843	0.000000	0.000000	-1852.787
-152.1300	0.000000		
0.000000	0.000000	0.000000	0.000000
0.000000	0.000000		
0.000000	0.000000	0.000000	0.000000
0.000000	0.000000		
109324.2	-5205.998	-7.625033	2.721410
-55031.80	1.7745042E-06		
0.000000	0.000000	0.000000	0.000000
0.000000	0.000000		
0.000000	0.000000	0.000000	0.000000
0.000000			

5280.904	2.721410	-4691.024	1.7745042E-06
-45.35775	0.000000		
0.000000	0.000000	0.000000	0.000000
0.000000	0.000000		
0.000000	0.000000	0.000000	
65955.29	1850.065	0.000000	0.000000
-33053.00	1.0778679E-06		
0.000000	0.000000	0.000000	0.000000
0.000000	0.000000		
0.000000	0.000000	0.000000	
4890.779	0.000000	0.000000	1.0778679E-06
-47.62442	0.000000		
0.000000	0.000000	0.000000	0.000000
0.000000	0.000000		
0.000000	0.000000	0.000000	
109324.2	5205.998	-7.625033	-2.721411
-54284.75	-5203.277		
0.000000	0.000000	0.000000	0.000000
0.000000	0.000000		
5280.904	-2.721411	-4691.024	-5203.277
-544.5213	0.000000		
0.000000	0.000000	0.000000	0.000000
0.000000			
65955.29	-1850.065	0.000000	0.000000
-32894.66	1852.787		
0.000000	0.000000	0.000000	0.000000
4890.779	0.000000	0.000000	1852.787
-152.1300	0.000000		
0.000000	0.000000	0.000000	
106432.1	15202.19	-5.326690	-3.293367
-52142.03	-9995.621		
0.000000	0.000000		
5782.588	-3.293367	-3274.865	-9995.621
-1963.201	0.000000		
0.000000			
65326.99	-5502.978	0.000000	0.000000
-32427.00	3653.484		
3886.843	0.000000	0.000000	3653.484
-459.8479			
101011.7	24055.02	-3.328782	-1.270904
8098.644	-1.270904	-2041.976	
64100.52	-9009.456		
3457.006			

Verificare – pentru elementul diagonal A_{55} :

Linia 5 a matricii (corespunzând la ΔU_{3x}), completată cu elementele 51 ... 54 (egale cu elementele 15 ... 45) este:

<u>-52142.03</u>	-1963.201	-32427.00	-459.8479
106432.1	-15202.19	<u>-5.326690</u>	3.293367
<u>-54284.75</u>	5203.277		

Suma elementelor non-diagonale corespunzând lui ΔU_{1x} , ΔU_{4x} și ΔU_{5x} (nodurile conectate cu 3 sunt 1, 4, 5), luate cu semn schimbat, este:

$$52142.03 + 5.326690 + 54284.75 = 106432.10669$$

■